

# Airfoil Shape Optimization Using Output-Based Adapted Meshes

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# Outline

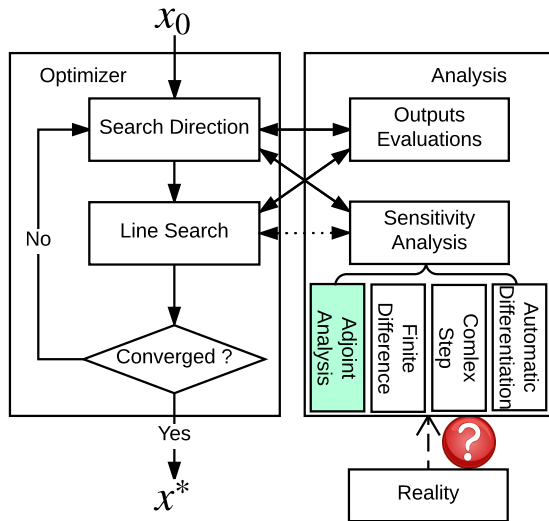
- 1 Introduction
- 2 Optimization Problem
- 3 Discretization
- 4 Error Estimation and Mesh Adaptation
- 5 Optimization Approach
- 6 Results and Discussion
- 7 Conclusions and Future Work



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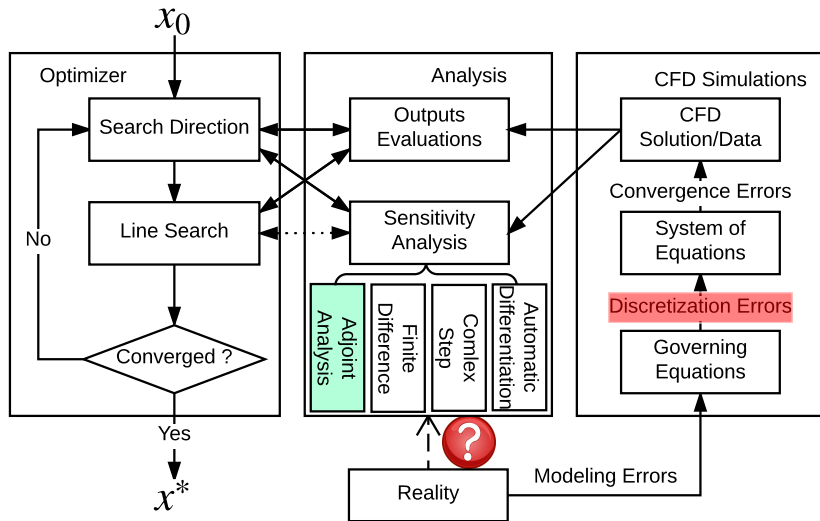
# Aerodynamic Shape Design/Optimization

## Design/Optimization: Numerical Optimization + CFD Analysis



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# Improving Optimization Accuracy and Efficiency

## Traditional methods

- a *priori* mesh: numerical error not controlled during optimization
- fixed fidelity: optimizing on fixed mesh resolution

## Proposed method

- Multi-fidelity optimization: reduce the computational resources at the early stages of optimization
- Adjoint based error estimation and mesh adaptation: actively control the numerical error during the optimization
- Integration) Multi-fidelity optimization driven by error estimation and mesh adaptation:  
Initial shape ) Optimal design, Coarse mesh ) Fine mesh  
*Goal: prevent over-refining and over-optimizing*



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# Optimization Problem Formulation

## General optimization problem

- Determine the design variables  $\mathbf{x}$  that minimize the objective function  $J$ :

$$\begin{aligned} \min_{\mathbf{x}} \quad & J(\mathbf{U}; \mathbf{x}) \\ \text{s.t.} \quad & \mathbf{R}^e(\mathbf{U}; \mathbf{x}) = \mathbf{0} \\ & \mathbf{R}^{ie}(\mathbf{U}; \mathbf{x}) \leq \mathbf{0} \end{aligned}$$

- $\mathbf{U}$  denotes the flow variables,  $\mathbf{R}^e$  and  $\mathbf{R}^{ie}$  are the equality and inequality constraints.

## Aerodynamic optimization

- Objective and constraints are aerodynamic outputs
- Physical feasibility: Flow variables  $\mathbf{U}$  are solved within a feasible design space to satisfy the flow equations,

$$\mathbf{R}(\mathbf{U}; \mathbf{x}) = \mathbf{0}; \quad \delta \mathbf{x} \geq 0$$





# Adjoint and Design Equations

## Objective and trim constraints

- Objective outputs: directly targeted for mesh adaptation, denoted as  $J^{\text{adapt}}$
- Trim constraints: We only consider the equality constraints  $\mathbf{R}^e$  and active inequality constraints  $\mathbf{R}_a^{\text{ie}}$ ,

$$\mathbf{R}^{\text{trim}} = [\mathbf{R}^e \ \mathbf{R}_a^{\text{ie}}]^T = \mathbf{J}^{\text{trim}} \quad \mathbf{J}^{\text{trim}} = \mathbf{0}$$

## Augmented Lagrangian functions

The adjoint-based optimization is equivalent to searching for the stationary point of the augmented Lagrangian function,

$$\mathcal{L}(\mathbf{U}; \mathbf{x}; \boldsymbol{\lambda}; \boldsymbol{\mu}) = J^{\text{adapt}}(\mathbf{U}; \mathbf{x}) + \boldsymbol{\lambda}^T \mathbf{R}(\mathbf{U}; \mathbf{x}) + \boldsymbol{\mu}^T \mathbf{R}^{\text{trim}}(\mathbf{U}; \mathbf{x})$$

where  $\boldsymbol{\lambda}$  and  $\boldsymbol{\mu}$  are Lagrange multipliers associated with the flow equations and the trim constraints, respectively



# Optimality Condition

- First-order optimality (Karush-Kuhn-Tucker) condition

$$\frac{\partial L}{\partial \mathbf{x}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} = \mathbf{0} \quad \text{optimal design}$$

$$\frac{\partial L}{\partial \mathbf{U}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \lambda^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0} \quad \text{coupled adjoint}$$

$$\frac{\partial L}{\partial \mathbf{U}} = \mathbf{R}(\mathbf{U}; \mathbf{x}) = \mathbf{0} \quad \text{physics feasibility}$$

$$\frac{\partial L}{\partial \mathbf{U}} = \mathbf{R}^{\text{trim}}(\mathbf{U}; \mathbf{x}) = \mathbf{0} \quad \text{trim condition}$$

- Always physically feasible:  $\mathbf{R}(\mathbf{U}; \mathbf{x}) = \mathbf{0}$
- Choose coupled adjoints variables, such that,

$$\left. \frac{\partial L}{\partial \mathbf{U}} = \mathbf{0} \right) \quad \lambda^T = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + \mu^T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} \quad \frac{\partial \mathbf{R}}{\partial \mathbf{U}}^T$$

$$= \left( \begin{array}{cc} \text{adapt} & + \quad \text{trim} \end{array} \right)^T$$



# Reduced optimality condition

- Coupled adjoints:  $T = ( \text{adapt} + \text{trim} )^T$ , where

$$\frac{\partial \mathbf{R}^T}{\partial \mathbf{U}} \text{adapt} + \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} = \mathbf{0}; \quad \frac{\partial \mathbf{R}^T}{\partial \mathbf{U}} \text{trim} + \frac{\partial J^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0}$$

- Sensitivity Analysis

$$\begin{aligned} \frac{\partial L}{\partial \mathbf{x}} &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} \\ &= \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + ( \text{adapt} )^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} + ( \text{trim} )^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} \\ &= \frac{dJ^{\text{adapt}}}{dx} + T \frac{dJ^{\text{trim}}}{dx} \end{aligned}$$

- Reduced optimality condition:

$$\begin{aligned} \frac{\partial L}{\partial \mathbf{x}} &= \frac{dJ^{\text{adapt}}}{dx} + T \frac{dJ^{\text{trim}}}{dx} = \mathbf{0} \\ \frac{\partial L}{\partial} &= \mathbf{R}^{\text{trim}} = \mathbf{0} \end{aligned}$$



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# Discretization

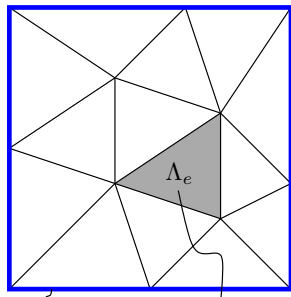
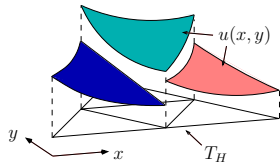
- Conservation law:  $\partial_t \mathbf{u} + r \mathbf{H}(\mathbf{u}; r \mathbf{u}) = \mathbf{0}$

where  $\mathbf{H} = \mathbf{F}(\mathbf{u}) + \mathbf{G}(\mathbf{u}; r \mathbf{u})$

total flux      inviscid flux      viscous flux

- DG approx of order  $p_e$  on each element:

$$\mathbf{u}_h(\mathbf{x}) = \sum_{e=1}^{N_e} \sum_{n=1}^{N_{p_e}} \mathbf{U}_{e;n} \phi_{e;n}(\mathbf{x})$$



domain  $\Omega$

element  $e$

$N_e$  = # of elements

$p_e$  = approx order on element  $e$

$N_{p_e}$  = # of basis fcn on element  $e$

$\phi_{e;n}(\mathbf{x})$  =  $n^{\text{th}}$  basis fcn of order  $p_e$  on  $e$

$\mathbf{U}_{e;n}$  = coefficients vector of  $n^{\text{th}}$  basis function on element  $e$



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# Output-Based Error Estimation

For a given configuration (design)  $\mathbf{x}$ , the outputs (objective and constraints) are based on a **pure** CFD flow solve.

**Output Error:**  $J = J_H(\mathbf{U}_H; \mathbf{x}) - J(\mathbf{U}; \mathbf{x})$

This is the difference between  $J$  computed with the discrete system solution,  $\mathbf{U}_H$ , and  $J$  computed with the *exact* solution,  $\mathbf{U}$ .

**Error Surrogate:**  $J = J_H(\mathbf{U}_H; \mathbf{x}) - J_h(\mathbf{U}_h; \mathbf{x})$

The difference between outputs on coarse and fine discretizations.

$$\text{coarse space: } \left\{ \begin{array}{l} \mathbf{R}_H(\mathbf{U}_H; \mathbf{x}) = \mathbf{0} \\ \{ \mathbf{Z} \} \\ N_H \text{ flow equations} \end{array} \right\} \left\{ \begin{array}{l} \mathbf{U}_H \\ \{ \mathbf{Z} \} \\ \text{state} \in \mathbb{R}^{N_H} \end{array} \right\} \quad J_H(\mathbf{U}_H; \mathbf{x})$$

$$\text{fine space: } \left\{ \begin{array}{l} \mathbf{R}_h(\mathbf{U}_h; \mathbf{x}) = \mathbf{0} \\ \{ \mathbf{Z} \} \\ N_h \text{ flow equations} \end{array} \right\} \left\{ \begin{array}{l} \mathbf{U}_h \\ \{ \mathbf{Z} \} \\ \text{state} \in \mathbb{R}^{N_h} \end{array} \right\} \quad J_h(\mathbf{U}_h; \mathbf{x})$$



# Adjoint-based Error Estimation

- State injection:  $\mathbf{U}_h^H = \mathbf{I}_h^H \mathbf{U}_H$
- $\mathbf{U}_h^H$  will generally not satisfy the fine-space equations,

$$\mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}) \neq \mathbf{0}$$

- Recall the definition of the output adjoint,  $\frac{\partial \mathbf{R}}{\partial \mathbf{U}}^T + \frac{\partial J}{\partial \mathbf{U}}^T = \mathbf{0}$ .  
relates the residual perturbation to an output perturbation,

$$J = \frac{\partial J}{\partial \mathbf{U}} \mathbf{U} = \underbrace{\left\{ \frac{\partial \mathbf{R}}{\partial \mathbf{U}}^T \right\}}_{\text{adjoint definition}} \underbrace{\left\{ \mathbf{U} \right\}}_{\text{residual linearization}} = \mathbf{R}^T \mathbf{R}$$

$$J = J_H(\mathbf{U}_H; \mathbf{x}) \quad J_h(\mathbf{U}_h; \mathbf{x}) = J_h(\mathbf{U}_h^H; \mathbf{x}) \quad J_h(\mathbf{U}_h; \mathbf{x})$$

$$\mathbf{R}_h^T \mathbf{R}_h = \mathbf{R}_h^T \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x})$$

- Error (Adapt) indicator: the error is localized in each element and serves as an adaptation indicator,  $e = j \mathbf{R}_{h,e}^T(\mathbf{U}_h^H; \mathbf{x}) j$





# Error Estimation and Mesh Adaptation for Optimization

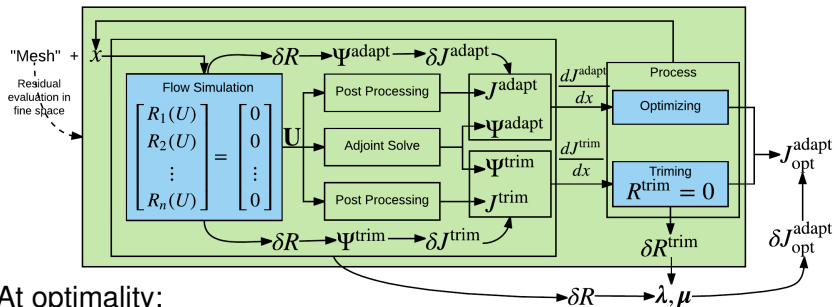
- Numerical error affects both objective and constraint outputs.
- How to estimate the error and adapt the mesh efficiently?
- Both errors can be obtained via adjoints.
- Possible adaptation strategies:
  - 1 Adapt only on the objective  
Error due to inexact constraints satisfaction
  - 2 Adapt equally on the objective and constraints  
Inefficient, expensive to keep all outputs very accurate
  - 3 Adapt on combined/weighted outputs  
The weights? Adapt more on objective/constraints?
  - 4 Adapt on the optimization problem (coupled adjoint)

coarse space:  $\mathbf{x}_0$  / optimization /  $\begin{matrix} \mathbf{x}_H \cdot \mathbf{U}_H \\ \hline \mathbf{z}_H \end{matrix}$  /  $J_H(\mathbf{U}_H; \mathbf{x}_H)$   
optimal design

fine space:  $\mathbf{x}_0$  / optimization /  $\begin{matrix} \mathbf{x}_h \cdot \mathbf{U}_h \\ \hline \mathbf{z}_h \end{matrix}$  /  $J_h(\mathbf{U}_h; \mathbf{x}_h)$   
optimal design



# Error Estimation and Mesh Adaptation for Optimization



$$\frac{\partial L}{\partial \mathbf{x}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} = 0$$

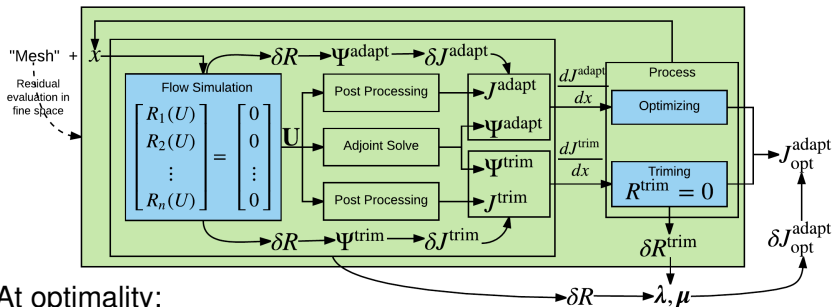
$$\frac{\partial L}{\partial \mathbf{U}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = 0$$

$$\frac{\partial L}{\partial \mathbf{x}} = \mathbf{R}(\mathbf{U}; \mathbf{x}) = 0$$

$$\frac{\partial L}{\partial \mathbf{x}} = \mathbf{R}^{\text{trim}}(\mathbf{U}; \mathbf{x}) = 0$$



# Error Estimation and Mesh Adaptation for Optimization



$$\begin{aligned}
 \mathcal{J}_{\text{opt}}^{\text{adapt}} &= \begin{matrix} T & T \\ h & h \end{matrix} \mathbf{R}_h \quad \mathbf{R}_h^{\text{trim}} \\
 &= \begin{matrix} T & T \\ h & h \end{matrix} \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}_H) \quad \mathbf{R}_h^{\text{trim}}(\mathbf{U}_h^H; \mathbf{x}_H) \\
 &= \left( \begin{matrix} \text{adapt} & \text{trim} \\ h & h \end{matrix} \right)^T \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}_H) \quad \begin{matrix} T \\ h \end{matrix} \left\{ \underbrace{\mathbf{J}_h^{\text{trim}}(\mathbf{U}_h^H; \mathbf{x}_H)}_0 \quad \mathbf{J}_h^{\text{trim}} \right\} \\
 &= \mathcal{J}^{\text{adapt}}(\mathbf{x}_H) + \begin{matrix} T \\ h \end{matrix} \mathbf{J}^{\text{trim}}(\mathbf{x}_H)
 \end{aligned}$$

Note:  $\mathbf{J}_h^{\text{trim}}(\mathbf{U}_h^H; \mathbf{x}_H) = \mathbf{J}_H^{\text{trim}}(\mathbf{U}_H; \mathbf{x}_H) = \mathbf{J}^{\text{trim}} = \mathbf{J}_h^{\text{trim}}(\mathbf{U}_h; \mathbf{x}_h)$



## Optimality error estimation

$$\frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \tau \frac{dJ^{\text{trim}}}{d\mathbf{x}} = \mathbf{0}$$

$$j_{\text{opt}}^{\text{adapt}} = \underbrace{j^{\text{adapt}}(\mathbf{x}_H)}_{\text{objective error only}} + \underbrace{\frac{\tau}{h} J^{\text{trim}}(\mathbf{x}_H)}_{\text{inexact constraints satisfaction}}$$

What does  $j_{\text{opt}}^{\text{adapt}}$  mean?

It is the objective sensitivity w.r.t constraints and measures how much the constraints error can affect the optimal objective.

## Mesh adaptation implementation

Adapt (error) indicator:  $j_{h_i}^T \mathbf{R}_{h_i} (\mathbf{U}_{h_i}^H; \mathbf{x}_H) j$

Combined indicator:  $j_{\text{opt}} = j^{\text{adapt}} + j^T j^{\text{trim}}$

$h_i$ : reconstructing the coarse-space adjoints  $H$

$h_i$ : extracted from the optimizer on the coarse space



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# Multi-fidelity Optimization with Error Control

## Geometry and Mesh

- Airfoil parameterization: Hicks-Henne basis function
- Design parameters: airfoil shape + angle of attack
- Mesh movement: Radial Basis Function (RBF) interpolation

## Optimization Algorithm

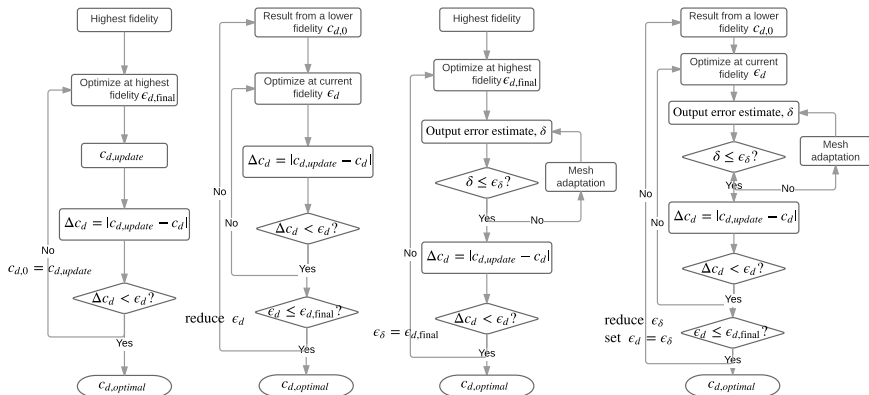
- Sequential Least Squares Programming (SLSQP)
- Broyden-Fletcher-Goldfarb-Shanno (BFGS) Hessian update
- Inexact line search: weak Wolfe condition



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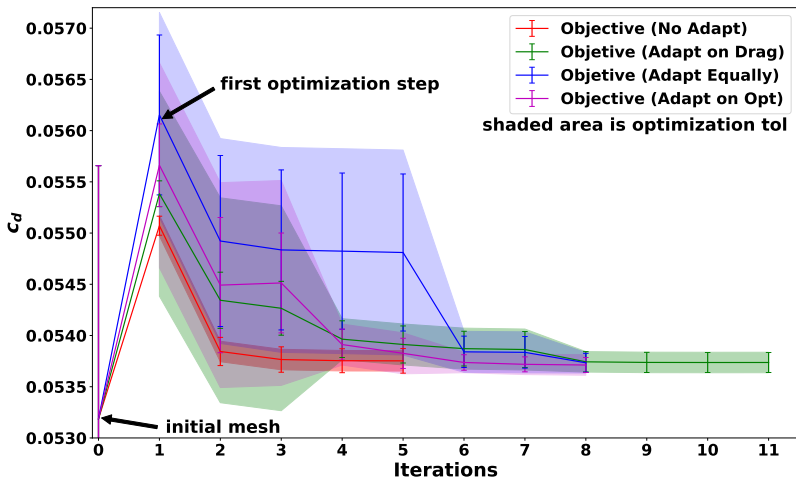
# Laminar, Subsonic Flow (nearly feasible starting point)

NACA 0012,  $Re = 5000$ ,  $M_1 = 0.5$ ,  $\alpha_0 = 0$   
 $J^{\text{adapt}} = C_d$ ,  $J^{\text{trim}} = C_l$ ,  $J^{\text{trim}} = 0.02$ ,  $A = A_{\text{min}}$



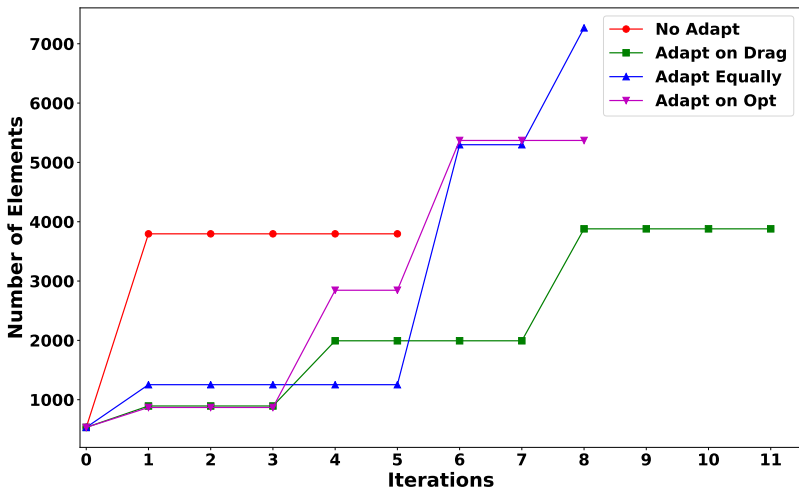
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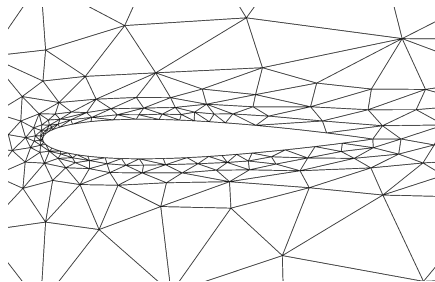


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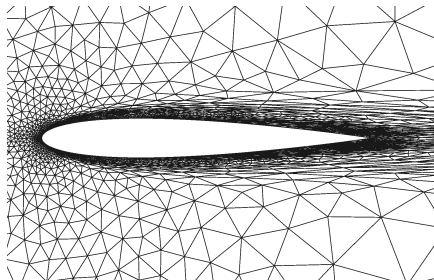


# Mesh Evolution



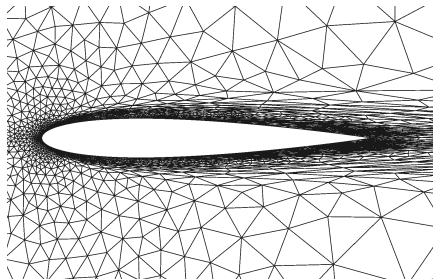
initial mesh (533 elements)

# Mesh Evolution

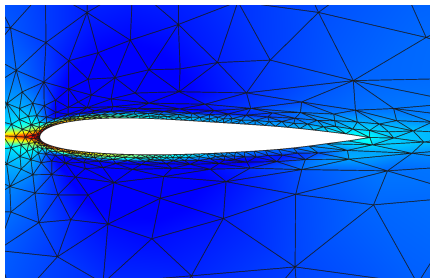


no adapt (3796 elements)

# Mesh Evolution

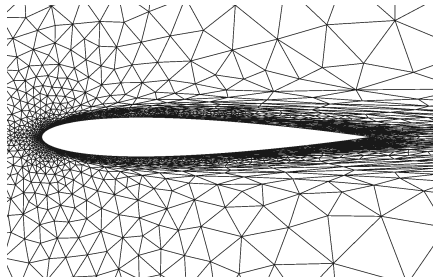


no adapt (3796 elements)

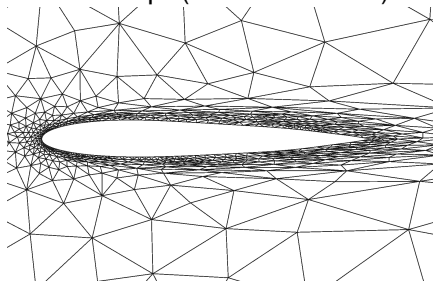


drag adapt (894 elems, adapt)

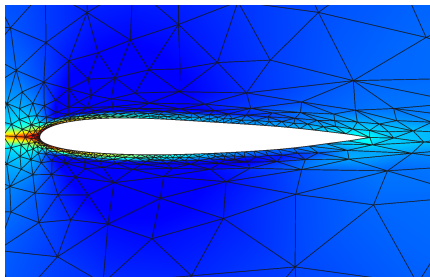
# Mesh Evolution



no adapt (3796 elements)

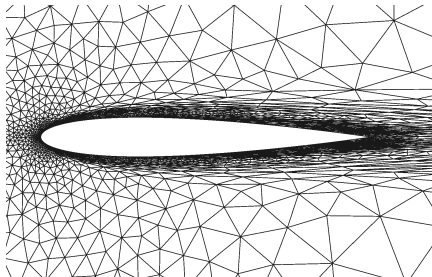


adapt equally (1253 elements)

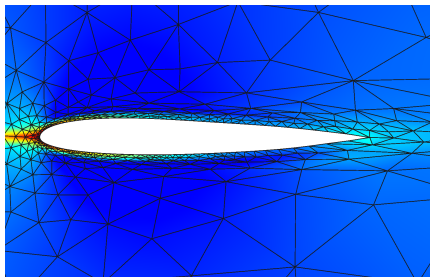


drag adapt (894 elems, adapt)

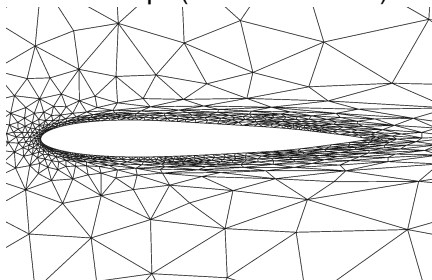
# Mesh Evolution



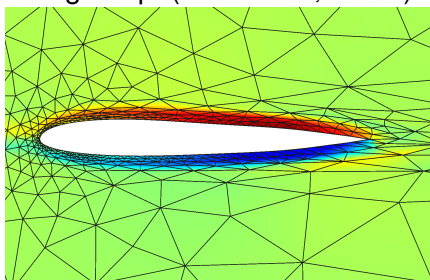
no adapt (3796 elements)



drag adapt (894 elems, adapt)



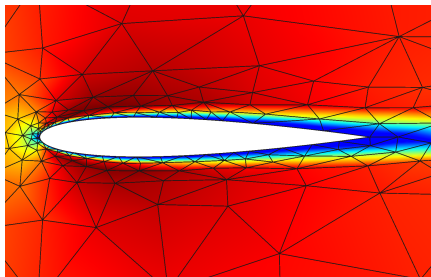
adapt equally (1253 elements)



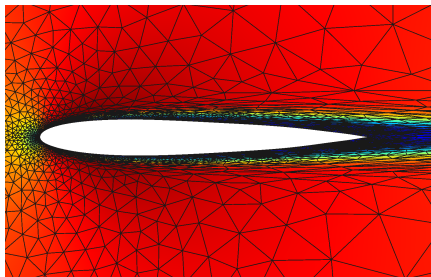
opt adapt (869 elems, trim)





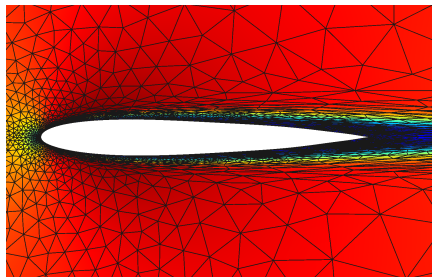


initial airfoil (  $\epsilon = 0$  )

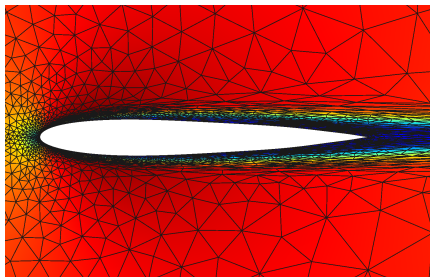


no adapt (  $\epsilon = 0.27$  )

# Optimized design (Mach Contour 0.6)

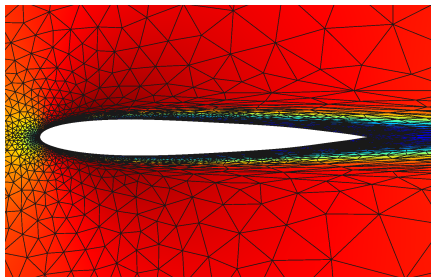


no adapt (  $C_D = 0.27$  )

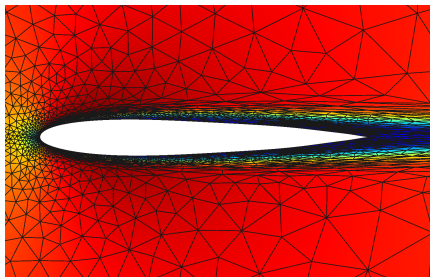


adapt on drag (  $C_D = 0.30$  )

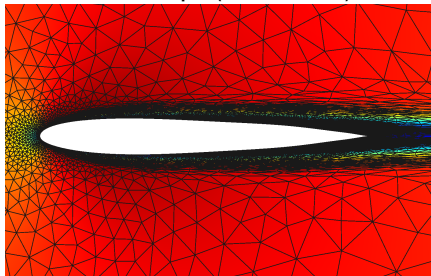
# Optimized design (Mach Contour 0 0:6)



no adapt (  $C_D = 0.27$  )



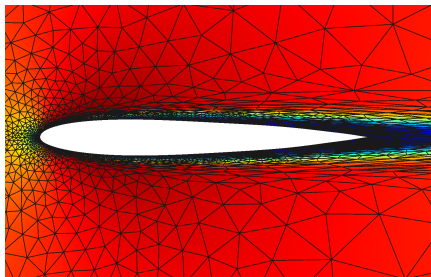
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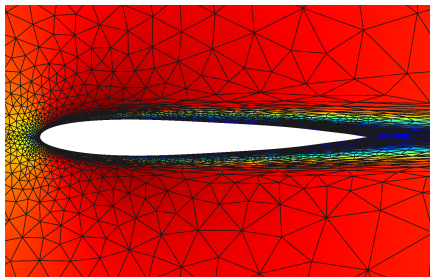
adapt equally (  $C_D = 0.25$  )



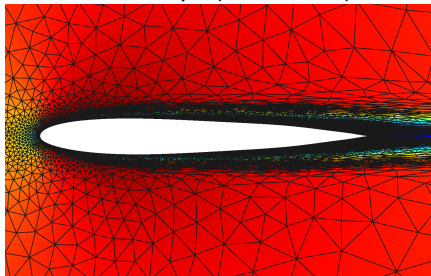
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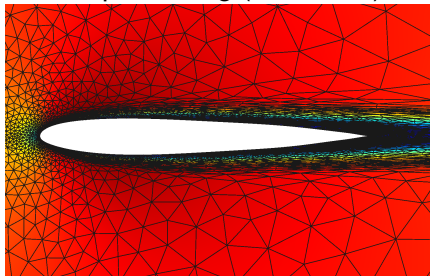
no adapt (  $C_D = 0.27$  )



adapt on drag (  $C_D = 0.30$  )



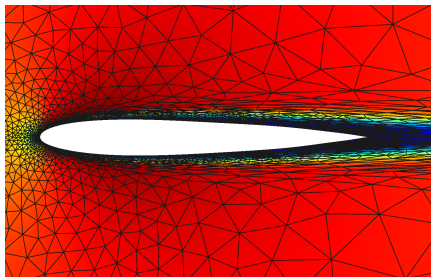
adapt equally (  $C_D = 0.25$  )



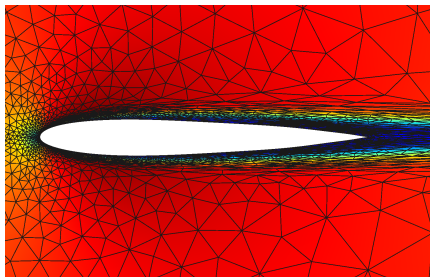
adapt on opt (  $C_D = 0.24$  )



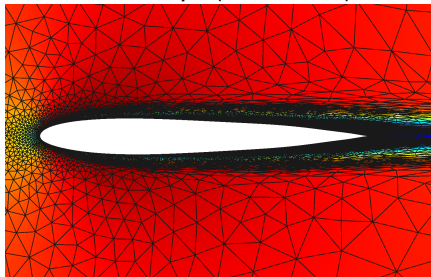
# Optimized design (Mach Contour 0 0:6)



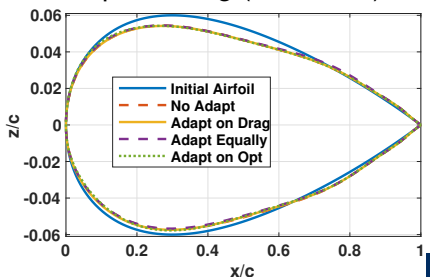
no adapt (  $C_d = 0.27$  )



adapt on drag (  $C_d = 0.30$  )



adapt equally (  $C_d = 0.25$  )

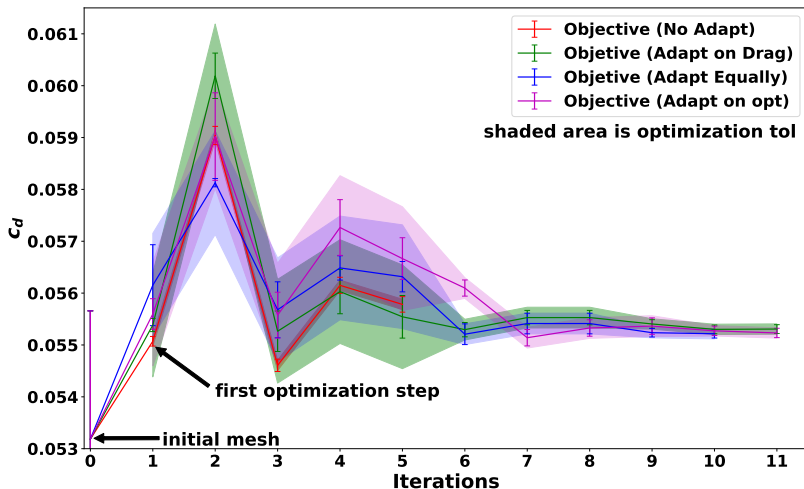


final design



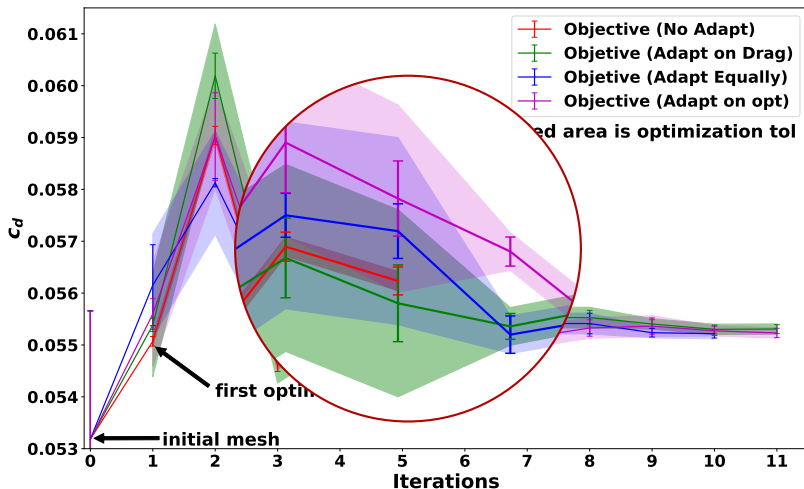
# Laminar, Subsonic Flow (infeasible starting point)

NACA 0012,  $Re = 5000$ ,  $M_1 = 0.5$ ,  $\alpha = 0$   
 $J_{\text{adapt}} = c_d$ ,  $J^{\text{trim}} = c_l$ ,  $J^{\text{trim}} = 0.1$ ,  $A = A_{\text{min}}$



# Laminar, Subsonic Flow (infeasible starting point)

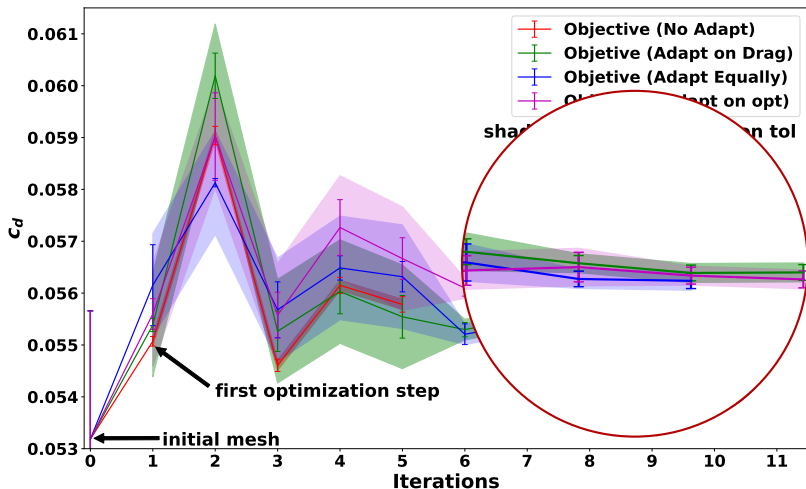
NACA 0012,  $Re = 5000$ ,  $M_1 = 0.5$ ,  $\alpha = 0$   
 $J_{\text{adapt}} = c_d$ ,  $J_{\text{trim}} = c_l$ ,  $J_{\text{trim}} = 0.1$ ,  $A = A_{\text{min}}$





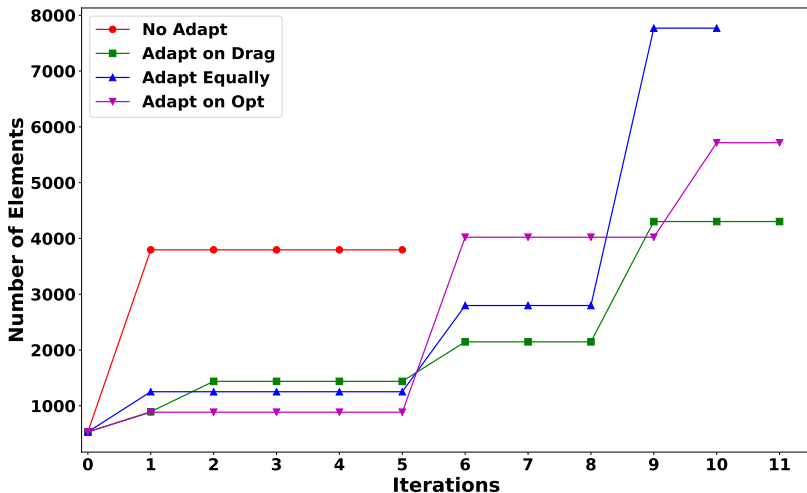
# Laminar, Subsonic Flow (infeasible starting point)

NACA 0012,  $Re = 5000$ ,  $M_1 = 0.5$ ,  $\alpha = 0$   
 $J_{\text{adapt}} = c_d$ ,  $J_{\text{trim}} = c_l$ ,  $J_{\text{trim}} = 0.1$ ,  $A = A_{\text{min}}$



# Laminar, Subsonic Flow (infeasible starting point)

NACA 0012,  $Re = 5000$ ,  $M_1 = 0.5$ ,  $\theta_0 = 0$   
 $J_{adapt} = c_d$ ,  $J_{trim} = c_l$ ,  $J_{trim} = 0.1$ ,  $A = A_{min}$



initial mesh (533 elements)

no adapt (3796 elements)

# Mesh Evolution

no adapt (3796 elements)

drag adapt (1439 elems, adapt)

# Mesh Evolution

no adapt (3796 elements)

drag adapt (1439 elems, adapt)

adapt equally (1253 elems)

# Mesh Evolution

no adapt (3796 elements)

drag adapt (1439 elems, adapt)

adapt equally (1253 elems)

opt adapt (886 elems, trim)

initial airfoil ( = 0 )



no adapt ( = 2:53 )

no adapt ( = 2:53 )

adapt on drag ( = 2:46 )

no adapt ( = 2:53 )

adapt on drag ( = 2:46 )

adapt equally ( = 2:39 )

no adapt ( = 2:53 )

adapt on drag ( = 2:46 )

adapt equally ( = 2:39 )

adapt on opt ( = 2:40 )

no adapt ( = 2:53 )

adapt on drag ( = 2:46 )

adapt equally ( = 2:39 )

nal design

# Inviscid, Transonic Flow

NACA 0012,  $M_1 = 0.8$ ,  $\theta_0 = 1:25$   
 $J^{\text{adapt}} = c_d$ ,  $J^{\text{trim}} = c_l$ ,  $J^{\text{trim}} = 0.4$ ,  $A = A_{\text{min}}$

# Turbulent, Low-Speed Flow

NACA 0012,  $Re = 10^6$ ,  $M_1 = 0.15$ ,  $\theta_0 = 6^\circ$   
 $J^{adapt} = c_d$ ,  $J^{trim} = c_l$ ,  $J^{trim} = 0.6$ ,  $A_{min}$

initial mesh

1st step mesh

final mesh

# Turbulent, Low-Speed Flow

NACA 0012,  $Re = 10^6$ ,  $M_1 = 0.15$ ,  $\alpha = 6^\circ$   
 $J^{adapt} = c_d$ ,  $J^{trim} = c_l$ ,  $J^{trim} = 0.6$ ,  $A = A_{min}$

initial design

nal design

airfoil shape



# Outline

- 1 Introduction
- 2 Optimization Problem
- 3 Discretization
- 4 Error Estimation and Mesh Adaptation
- 5 Optimization Approach
- 6 Results and Discussion
- 7 **Conclusions and Future Work**

# Conclusion

## Conclusions:

Numerical error should be carefully controlled as the shape and mesh change during the optimization

We integrate output-based error estimation and mesh adaptation with a traditional gradient-based algorithm

Error tolerance serves as the optimization tolerance at each delity, delity increases through mesh adaptation.

Coupled adjoint error estimation offers a more efficient way to adapt the mesh for constrained optimization problem

Prevent over-refinement and over-optimizing during optimization

## Future Work:

Develop improved and automated delity increase strategy

Avoid overshoot refinement, allow more mesh redistribution and coarsening, optimize mesh during the optimization

Combined with h-p refinement

# Acknowledgments

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Boeing Company, with technical monitor Dr. Mori Mani  
— Thank you —

# Sensitivity Verification

# Adapt Indicator

# Complete Error Estimation



# Error Estimation and Mesh Adaptation for Optimization



Flow problem:

$$\begin{aligned} J &= J_h(\mathbf{U}_h^H; \mathbf{x}) = J_h(\mathbf{U}_h; \mathbf{x}) \\ &= \mathbf{R}_h^T \\ &= \mathbf{R}_h^T(\mathbf{U}_h^H; \mathbf{x}) \end{aligned}$$





Flow problem:

$$\begin{aligned} J &= J_h(\mathbf{U}_h^H; \mathbf{x}) = J_h(\mathbf{U}_h; \mathbf{x}) \\ &= \mathbf{R}_h^T \\ &= \mathbf{R}_h^T(\mathbf{U}_h^H; \mathbf{x}) \end{aligned}$$

During optimization:



# Error Estimation and Mesh Adaptation for Optimization

Flow problem:

$$\begin{aligned} J &= J_h(\mathbf{U}_h^H; \mathbf{x}) = J_h(\mathbf{U}_h; \mathbf{x}) \\ &= \mathbf{R}_h^T \mathbf{R}_h \\ &= \mathbf{R}_h^T \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}) \end{aligned}$$

During optimization:

$$\begin{aligned} \frac{\partial L}{\partial \mathbf{x}} &= \frac{\partial J_{\text{adapt}}}{\partial \mathbf{x}} + \mathbf{R}^T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + \mathbf{R}^{\text{trim}T} \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} \neq \mathbf{0} \\ \frac{\partial L}{\partial \mathbf{U}} &= \frac{\partial J_{\text{adapt}}}{\partial \mathbf{U}} + \mathbf{R}^T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + \mathbf{R}^{\text{trim}T} \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = \mathbf{0} \\ \frac{\partial L}{\partial \mathbf{U}} &= \mathbf{R}(\mathbf{U}; \mathbf{x}) = \mathbf{0} \\ \frac{\partial L}{\partial \mathbf{U}} &= \mathbf{R}^{\text{trim}}(\mathbf{U}; \mathbf{x}) \neq \mathbf{0} \end{aligned}$$



# Error Estimation and Mesh Adaptation for Optimization

Flow problem:

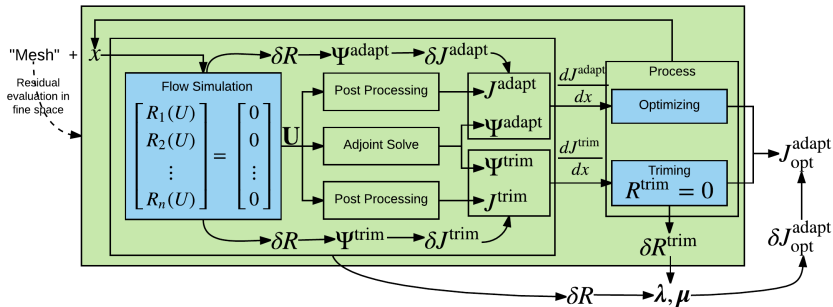
$$\begin{aligned}
 J &= J_h(\mathbf{U}_h^H; \mathbf{x}) = J_h(\mathbf{U}_h; \mathbf{x}) \\
 &= \mathbf{R}_h^T \mathbf{R}_h \\
 &= \mathbf{R}_h^T(\mathbf{U}_h^H; \mathbf{x})
 \end{aligned}$$

During optimization:

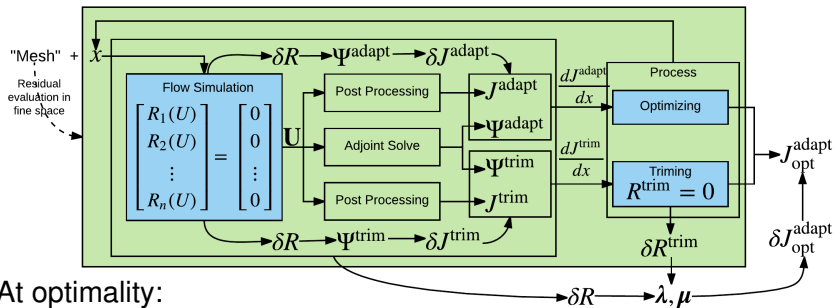
$$\begin{aligned}
 \mathcal{J}^{\text{adapt}} &= \mathbf{R}_h^T \mathbf{R}_h + \mathbf{R}_h^{\text{trim}T} \mathbf{R}_h^{\text{trim}} \\
 &= \mathbf{R}_h^T(\mathbf{U}_h^H; \mathbf{x}) + \mathbf{R}_h^{\text{trim}T}(\mathbf{U}_h^H; \mathbf{x}) \\
 &= \left( \mathcal{J}_h^{\text{adapt}} + \mathcal{J}_h^{\text{trim}} \right) \mathbf{R}_h^T(\mathbf{U}_h^H; \mathbf{x}) = \mathcal{J}_h^{\text{trim}}(\mathbf{U}_h^H; \mathbf{x}) + \mathcal{J}_h^{\text{trim}}(\mathbf{U}_h; \mathbf{x}) \\
 &= \mathcal{J}^{\text{adapt}} + \mathbf{R}_h^T \left\{ \underbrace{\mathbf{R}_h^{\text{trim}}(\mathbf{U}_h^H; \mathbf{x})}_{\mathcal{J}^{\text{trim}}} \right\} = \mathcal{J}^{\text{trim}} \\
 &= \mathcal{J}^{\text{adapt}}
 \end{aligned}$$



# Error Estimation and Mesh Adaptation for Optimization



# Error Estimation and Mesh Adaptation for Optimization



$$\frac{\partial L}{\partial \mathbf{x}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}}{\partial \mathbf{x}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{x}} = 0$$

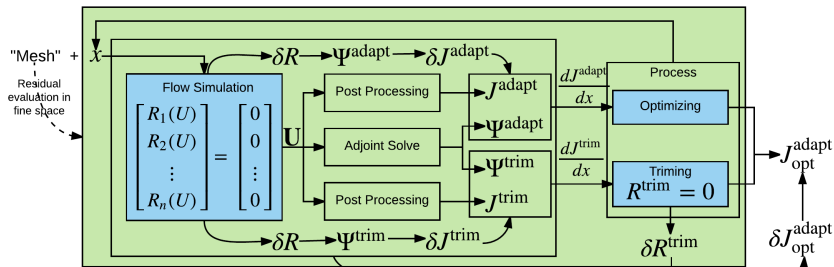
$$\frac{\partial L}{\partial \mathbf{U}} = \frac{\partial J^{\text{adapt}}}{\partial \mathbf{U}} + T \frac{\partial \mathbf{R}}{\partial \mathbf{U}} + T \frac{\partial \mathbf{R}^{\text{trim}}}{\partial \mathbf{U}} = 0$$

$$\frac{\partial L}{\partial \mathbf{x}} = \mathbf{R}(\mathbf{U}; \mathbf{x}) = 0$$

$$\frac{\partial L}{\partial \mathbf{x}} = \mathbf{R}^{\text{trim}}(\mathbf{U}; \mathbf{x}) = 0$$



# Error Estimation and Mesh Adaptation for Optimization



At optimality:

$$\begin{aligned}
 \mathcal{J}_{opt}^{adapt} &= \begin{matrix} T \\ h \end{matrix} \mathbf{R}_h \quad \begin{matrix} T \\ h \end{matrix} \mathbf{R}_h^{trim} \\
 &= \begin{matrix} T \\ h \end{matrix} \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}_H) \quad \begin{matrix} T \\ h \end{matrix} \mathbf{R}_h^{trim}(\mathbf{U}_h^H; \mathbf{x}_H) \\
 &= \left( \begin{matrix} adapt \\ h \end{matrix} + \begin{matrix} trim \\ h \end{matrix} \right)^T \mathbf{R}_h(\mathbf{U}_h^H; \mathbf{x}_H) \quad \begin{matrix} T \\ h \end{matrix} \left( \underbrace{\mathcal{J}_h^{trim}(\mathbf{U}_h^H; \mathbf{x}_H)}_0 \right) \\
 &= \mathcal{J}^{adapt}(\mathbf{x}_H) + \begin{matrix} T \\ h \end{matrix} \mathcal{J}^{trim}(\mathbf{x}_H)
 \end{aligned}$$

Note:  $\mathcal{J}_h^{trim}(\mathbf{U}_h^H; \mathbf{x}_H) = \mathcal{J}_H^{trim}(\mathbf{U}_H; \mathbf{x}_H) = \mathcal{J}^{trim} = \mathcal{J}_h^{trim}(\mathbf{U}_h; \mathbf{x}_h)$



## Optimality error estimation

$$\frac{dJ^{\text{adapt}}}{d\mathbf{x}} + \tau \frac{dJ^{\text{trim}}}{d\mathbf{x}} = \mathbf{0}$$

$$J_{\text{opt}}^{\text{adapt}} = J^{\text{adapt}}(\mathbf{x}_H) + \tau \frac{J^{\text{trim}}(\mathbf{x}_H)}{h}$$

What does  $J_{\text{opt}}^{\text{adapt}}$  mean?

It is the objective sensitivity w.r.t constraints and measures how much the constraints error can affect the optimal objective.

## Mesh adaptation implementation

Adapt (error) indicator:  $J_{h; \mathbf{R}_h; (\mathbf{U}_h^H; \mathbf{x}_H)}^{\text{adapt}}$

Combined indicator:  $J_{\text{opt}} = J_{\{Z\}}^{\text{adapt}} + \tau \frac{J_{\{Z\}}^{\text{trim}}}{h}$   
 objective error only      inexact constraints satisfaction

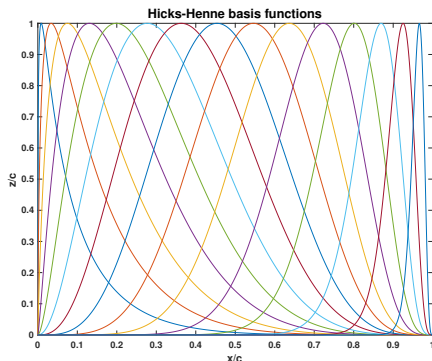
$h$ : reconstructing the coarse-space adjoints  $H$

$h$ : extracted from the optimizer on the coarse space



# Airfoil Parameterization

- Hicks-Henne basis functions: linear combination of "bump" functions added to the baseline airfoil



$$Z = Z_{\text{base}} + \sum_{i=0}^n a_i i(x)$$
$$i(x) = \sin^{t_i} (x^{m_i})$$
$$m_i = \ln(0.5) = \ln(x_{M_i})$$

$x$  : coord along the airfoil chord  
 $z$  : vertical surface coord  
 $x_{M_i}$  : maxima location  
 $t_i$  : width of the bump function

- Design parameters:  $\mathbf{x} = [ \alpha; a_1; a_2; \dots; a_n ]^T$   
Coefficients of Hicks-Henne basis + angle of attack



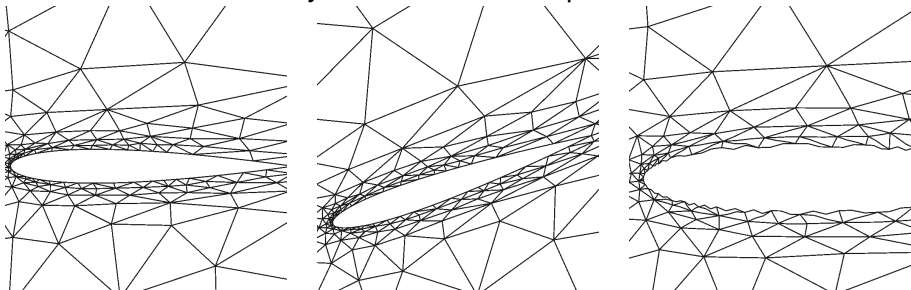


# Mesh Movement

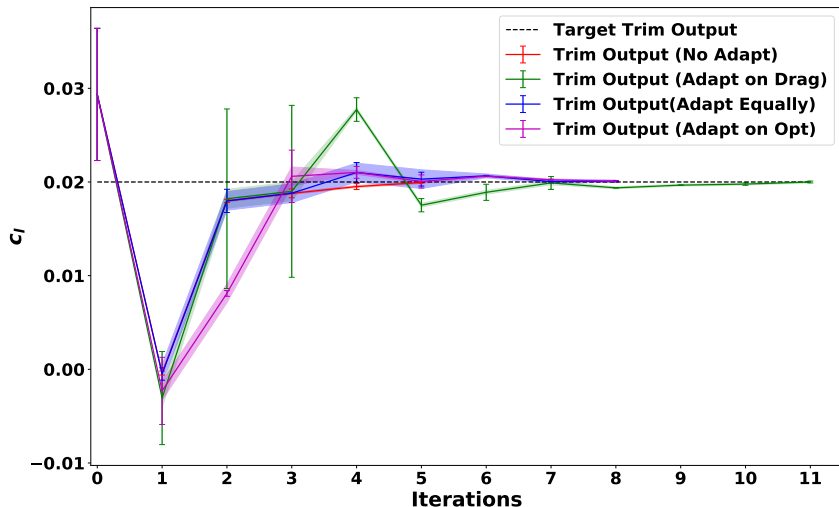
- Radial Basis Function (RBF): only depends on the distance from the origin or a center, e.g.  $\phi(x) = e^{-\alpha \|x\|^2}$
- We can use a sum of RBFs  $\phi(x; x_j)$  and a polynomial  $p(x)$  to interpolate the original function (mesh movement):

$$d(x) \quad d(x) = \sum_{i=1}^{N_b} f_i \phi(x; x_j) + p(x)$$

- Solving for a linear system  $O(N_b)$  of  $f_i$
- Mesh connectivity information not required



# Constraints, Nearly Feasible Starting Point



# Constraints, Infeasible Starting Point

